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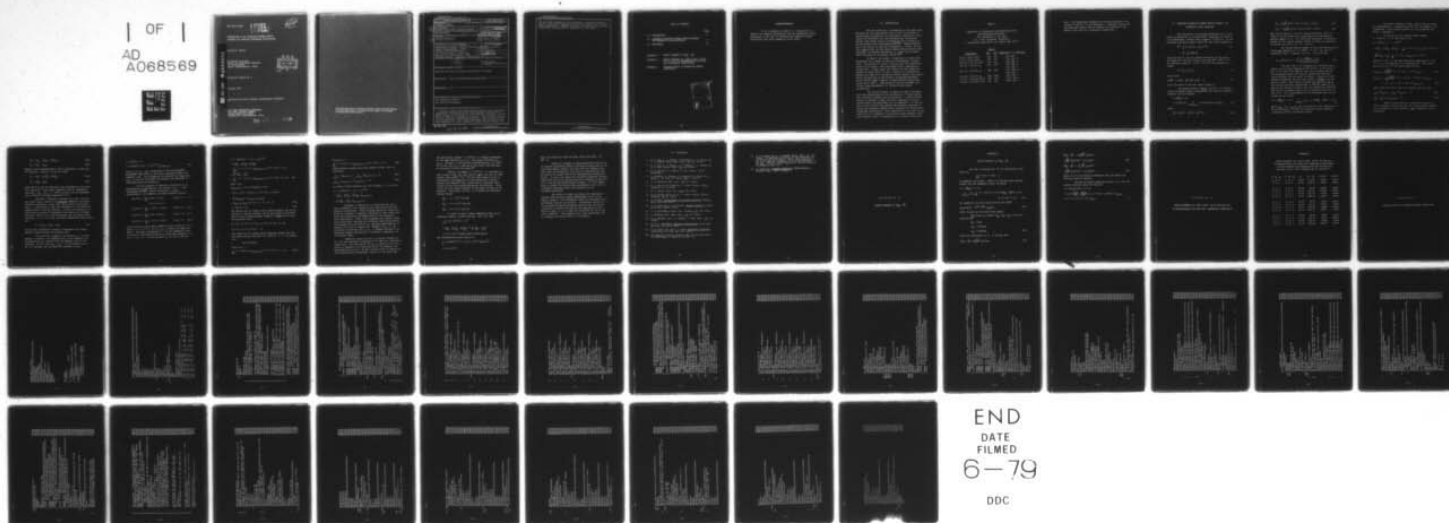
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COMPUTATION OF  $H_2O$  QUADRUPOLE MOMENT MATRIX  
ELEMENTS FOR PRESSURE BROADENING CALCULATIONS

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$H_2O$  and other asymmetric rotor molecules. Computer programs to obtain these matrix elements have been constructed and are presently operational. Numerical results for some low J quadrupole transitions are presented in Appendix B of the report. ↗

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## 1.0 INTRODUCTION

The work which will be presented in this report was motivated by our observations that, if only the effects of dipole-dipole interactions are considered, theoretical calculations of halfwidths for self-broadened  $H_2O$  transitions exhibit some rather serious discrepancies with recently reported tunable laser measurements.<sup>1,2,3,4/</sup> These discrepancies occur mainly at high and intermediate  $J$  values, and obtain using either the well-known Anderson-Tsao-Curnutte (ATC) theory<sup>5,6/</sup> of pressure broadening, or a more recent method (QFT) developed by the present author.<sup>7,8/</sup>

In Table I we present a comparison of theory with experiment for a number of high and intermediate  $J$  transitions. The results in Table I indicate that the theoretical widths are too small, with percentage errors sometimes exceeding 50%. In most cases the results are only weakly dependent on which theory is used. However, all theoretical numbers are based on a calculation which includes only dipole-dipole interactions as the dominant scattering mechanism. These results suggest neglect of some important scattering mechanism at high  $J$ . Some possibilities are exchange scattering, dipole-quadrupole, or dipole-induced-dipole interactions.

Our initial efforts to remove the above discrepancies have concentrated on the contribution of dipole-quadrupole collisions between the  $H_2O$  molecules. A future journal article is planned in which detailed comparison of the expanded theory with experiment will be presented. In this report we will outline the computational methods necessary to obtain  $H_2O$  quadrupole moment matrix elements for the pressure-broadening calculations. This computation is far from trivial since  $H_2O$  is an asymmetric top molecule whose permanent quadrupole moment cannot be represented by a single scalar quan-

TABLE I

Comparison of Theoretical and Experimental H<sub>2</sub>O  
Self-Broadened Halfwidths

(All halfwidths in cm<sup>-1</sup>/atm;

rot = pure rotational transition;

† measurement near 382°K, all others near 297°K)

<u>Transition</u>	<u>Theory</u>		<u>Experiment and Reference</u>
	<u>ATC</u>	<u>QFT</u>	
8,1,8 → 9,4,5 (rot)	.409	.402	.559, Ref. 5
8,3,6 → 9,6,3 (rot)	.343	.377	.611, Ref. 3
11,1,10 → 12,4,9 (rot)	.261	.257	.319, Ref. 3
12,2,11 → 13,1,12 v <sub>2</sub>	.160	.140	.228, Ref. 2
			.170, Ref. 4
15,1,15 → 16,0,16 v <sub>2</sub>	.098	.083	.177, Refs. 1, 2
			.166, Ref. 4
15,2,14 → 16,1,15 v <sub>2</sub>	.084	.085	.203, Ref. 2
17,0,17 → 18,3,16 (rot)	.085	.078	.125†, Ref. 3
19,0,19 → 20,3,18 (rot)	.063	.063	.089†, Ref. 3

tity. The theoretical framework for the calculations is developed in Section 2.0 and Appendix A. Numerical results for  $\text{H}_2\text{O}$  quadrupole moment matrix elements are presented in Appendix B for some low  $J$  quadrupole transitions.



## 2.0 PERMANENT QUADRUPOLE MOMENT MATRIX ELEMENTS FOR ASYMMETRIC ROTOR MOLECULES

The calculation of pressure broadening due to quadrupole interactions can be expressed<sup>7/</sup> completely in terms of an m-independent, reduced matrix element,  $\langle J || Q^t || J' \rangle$ , of the traceless quadrupole moment tensor  $\hat{Q}^t$ , the latter defined as

$$\hat{Q}^t = \sum_i e_i [\vec{r}_i \vec{r}_i - \frac{1}{3} r_i^2 \hat{I}], \quad (1)$$

$$= \hat{Q} - \frac{1}{3} \text{Tr}(\hat{Q}) \hat{I}, \quad (2)$$

where the sum is over all charged particles in the molecule, and where  $\hat{I}$  is the unit tensor, such that  $\hat{I} \cdot \vec{A} = \vec{A} \cdot \hat{I} = \vec{A}$  for an arbitrary vector  $\vec{A}$ . In Eq. (2),  $\hat{Q}$  is the quadrupole moment tensor

$$\hat{Q} = \sum_i e_i \vec{r}_i \vec{r}_i, \quad (3)$$

and we note

$$\text{Tr}(\hat{Q}^t) = \text{Tr}(\hat{Q}) - \frac{1}{3} \text{Tr}(\hat{Q}) \text{Tr}(\hat{I}) = 0, \quad (4)$$

since the trace of the unit tensor equals 3.

The reduced matrix element  $\langle J || Q^t || J' \rangle$  is defined using the Wigner-Eckhart theorem<sup>9,10/</sup> for traceless symmetric tensors, via the equation

$$\begin{aligned} & \langle J m | \hat{Q}^t | J' m' \rangle \\ &= \langle J || Q^t || J' \rangle \sum_{M=0, \pm 1, \pm 2} (J' 2 - m' - M | J' 2 J - m) \hat{T}_M, \end{aligned} \quad (5)$$

where

$$\hat{T}_0 = \frac{2}{3} [\hat{Z} \hat{Z} - \frac{1}{2} \hat{X} \hat{X} - \frac{1}{2} \hat{Y} \hat{Y}], \quad (5a)$$

$$\hat{T}_{\pm 2} = \frac{1}{2} \sqrt{\frac{2}{3}} [(\hat{X} \hat{X} - \hat{Y} \hat{Y}) \mp i(\hat{X} \hat{Y} + \hat{Y} \hat{X})], \quad (5b)$$

$$\hat{T}_{\pm 1} = \mp \frac{1}{2} \sqrt{\frac{2}{3}} [(\hat{Z} \hat{X} + \hat{X} \hat{Z}) \mp i(\hat{Z} \hat{Y} + \hat{Y} \hat{Z})]. \quad (5c)$$

Here (X,Y,Z) refer to a set of spaced-fixed axes, and Z is taken to be the direction of quantization for the magnetic quantum numbers m, m'. For non-linear molecules |J> actually stands for all quantum numbers (except m) which are necessary to specify the state, i.e. |J> = |Jτ...>.

The reduced matrix element is then obtained by calculating any component of  $\langle J \tau m | \hat{Q}^t | J' \tau' m' \rangle$ , e.g. the  $\hat{Z} \hat{Z}$  component, which is diagonal in m, m'. Thus, we have

$$\langle J \tau || \hat{Q}^t || J' \tau' \rangle = \frac{3}{2} \frac{\langle J \tau m | \hat{Q}_{ZZ}^t | J' \tau' m \rangle}{(J'2-m \ 0 | J'2 \ J-m)} \quad (6)$$

The next step is to transform to a principal axis system (x,y,z) which diagonalizes  $\hat{Q}^t$  and  $\hat{Q}$ . In the case of H<sub>2</sub>O, it is clear from symmetry that the principal axes for the quadrupole moment and inertial tensors are identical except possibly for the choice of origin. However, in most pressure-broadening theories this choice is fixed to be the center of mass. This results because one typically writes the various multipole interactions as  $V(\vec{R}_i - \vec{R}_j)$  where  $\vec{R}_i, \vec{R}_j$  specify the centers of mass of the two interacting molecules. This point is somewhat subtle and is discussed more fully in Ref. (17). The transformation to the principal axis (x,y,z) system can be written

$$\langle J \tau m | \hat{Q}_{ZZ}^t | J' \tau' m \rangle = \sum_{\alpha=x,y,z} Q_{\alpha\alpha} \langle J \tau m | [\hat{\Phi}_{Z\alpha}^2 - \frac{1}{3}] | J' \tau' m \rangle, \quad (7)$$

where  $Q_{\alpha\alpha} = \sum_i e_i r_{i\alpha} r_{i\alpha}$  are the principal axis components of  $\hat{Q}$ , and where  $\hat{\Phi}_{Z\alpha} = \hat{Z} \cdot \hat{a}$  are the direction cosine operators connecting the two coordinate systems.

The matrix elements of  $[\Phi_{Z\alpha}^2 - \frac{1}{3}]$  can be evaluated by transforming to a representation  $|J K m\rangle$  of symmetric top eigenstates. Some further details of this evaluation are given in Appendix A.

The result for the reduced matrix element  $\langle J \tau || Q^t || J' \tau' \rangle$  is then found to be

$$\langle J \tau || Q^t || J' \tau' \rangle = (-1)^{J+J'}$$

$$\cdot \left\{ (Q_{zz} - \frac{1}{2} Q_{xx} - \frac{1}{2} Q_{yy}) \cdot \sum_{KK'} \langle J \tau | J K \rangle A_{JK;J'K'} \langle J' K' | J' \tau' \rangle \right. \\ \left. - \sqrt{\frac{3}{4}} (Q_{xx} - Q_{yy}) \sum_{KK'} \langle J \tau | J K \rangle B_{JK;J'K'} \langle J' K' | J' \tau' \rangle \right.$$

where  $\langle J' K' | J' \tau' \rangle$  are the eigenvector components of state  $|J' \tau' \rangle$  in the symmetric top representation. The A and B matrices in Eq. (7) are given explicitly by

$$A_{JK;J'K'} = \sqrt{\frac{2J'+1}{2J+1}} (J' \ 2 \ K' \ 0 | J' \ 2 \ J \ K') \delta_{K,K'}, \quad (9a)$$

$$B_{JK;J'K'} = \frac{1}{\sqrt{2}} \sqrt{\frac{2J'+1}{2J+1}} \{ (J' \ 2 \ K' \ 2 | J' \ 2 \ J(K'+2)) \delta_{K,K'+2} \\ + (J' \ 2 \ K' \ -2 | J' \ 2 \ J(K'-2)) \delta_{K,K'-2} \}, \quad (9b)$$

and it may be verified that A, B satisfy the sum rules

$$\sum_{J'K'} A^2_{JK;J'K'} = \sum_{J'K'} B^2_{JK;J'K'} = 1, \quad (10a)$$

$$\sum_{J'K'} A_{JK;J'K'} B_{JK;J'K'} = 0. \quad (10b)$$

Several points should be noted before going on. First, from Eq. (8) we note that the reduced matrix element for an asymmetric rotor depends on two independent scalar parameters



$$Q_1 = (Q_{zz} - \frac{1}{2} Q_{xx} - \frac{1}{2} Q_{yy}), \quad (11a)$$

$$Q_2 = (Q_{xx} - Q_{yy}). \quad (11b)$$

However, this parameterization can be expressed in other useful fashions. From Eq. (2) we note that

$$Q_1 = (Q_{zz}^t - \frac{1}{2} Q_{xx}^t - \frac{1}{2} Q_{yy}^t), \quad (12a)$$

$$Q_2 = (Q_{xx}^t - Q_{yy}^t), \quad (12b)$$

where the  $Q^t$ 's are the principal axis components of the traceless tensor  $\hat{Q}^t$ . These three components are not independent since  $Q_{xx}^t + Q_{yy}^t + Q_{zz}^t = 0$ . Hence  $Q_1$  and  $Q_2$  can be parameterized in terms of any two components of  $Q^t$ .

Secondly, it should be pointed out in Eq. (8) that the labels (x,y,z) refer to an arbitrary symmetric top representation (arbitrary, except that (x,y,z) must be principal axes). In particular, z need not correspond to the (two-fold) symmetry axis of the  $H_2O$  molecule. In fact the numerical results which we present in Appendix B are based on a IR representation, where (z,x,y) are associated with the lowest-order constants,  $A > B > C$ , in the rotational-vibrational Hamiltonian via

$$H = B J_x^2 + C J_y^2 + A J_z^2. \quad (13)$$

For  $H_2O$  the intermediate constant B represents the inverse moment of inertia about the symmetry axis.

Of course for a symmetric top molecule, it is most natural to choose z, the symmetry axis of the symmetric top representation, to coincide with the symmetry axis of the molecule. In this case  $(Q_{xx} - Q_{yy}) = 0$ , the second term in Eq. (8) vanishes, and the equation collapses to give

$$\begin{aligned}
& \langle J \tau || Q^t || J' \tau' \rangle \\
& = \langle J K || Q^t || J' K' \rangle = (-1)^{J'+J} Q_1 A_{JK;J'K'}, \quad (14)
\end{aligned}$$

where  $Q_1 = (Q_{zz} - Q_{xx})$  corresponds to the Buckingham<sup>11/</sup>, Birnbaum<sup>12/</sup> definition of the scalar quadrupole moment for symmetric tops. This definition is one-half the value used, e.g., by Tsao and Curnutte<sup>6/</sup> and Benedict and Kaplan<sup>13/</sup> in discussing pressure-broadening.

For the purposes of numerical computation it is advantageous to transform Eq. (8) further using the Wang transformation<sup>14,15/</sup>, which corresponds to forming combinations of the symmetric top wave functions according

$$|E_+(J K)\rangle = \frac{1}{\sqrt{2}} \{ |J K\rangle + |J-K\rangle \} \quad K \text{ even} > 0, \quad (15a)$$

$$= |J 0\rangle \quad (K = 0)$$

$$|E_-(J K)\rangle = \frac{1}{\sqrt{2}} \{ - |J K\rangle + |J-K\rangle \} \quad K \text{ even} > 0, \quad (15b)$$

$$|O_+(J K)\rangle = \frac{1}{\sqrt{2}} \{ |J K\rangle + |J-K\rangle \} \quad K \text{ odd} > 0, \quad (15c)$$

$$|O_-(J K)\rangle = \frac{1}{\sqrt{2}} \{ - |J K\rangle + |J-K\rangle \} \quad K \text{ odd} > 0. \quad (15d)$$

Let us write the above Wang (symmetric top) states as  $|J K v\rangle$  where  $v = 1, 2, 3, 4 = E_+, E_-, O_+, O_-$  denotes the Wang symmetry. The exact eigenstates  $|J \tau\rangle$  of the asymmetric rotor can also be classified according to their Wang symmetry, i.e.  $|J \tau\rangle = |J \tau v\rangle$ . In this notation Eq. (8) can be written

$$\begin{aligned}
\langle J \tau v || Q^t || J' \tau' v' \rangle &= (-1)^{J'+J} \\
&\cdot \left\{ (Q_{zz}^t - \frac{1}{2} Q_{xx}^t - \frac{1}{2} Q_{yy}^t) \right. \\
&\cdot \sum_{K, K'} \langle J \tau v | J K v \rangle A_{JKv; J' K' v'} \langle J' K' v' | J' \tau' v' \rangle \\
&- \sqrt{\frac{3}{4}} (Q_{xx}^t - Q_{yy}^t) \\
&\cdot \sum_{KK'} \langle J \tau v | J K v \rangle B_{JKv; J' K' v'} \langle J' K' v' | J' \tau' v' \rangle \left. \right\}. \quad (16)
\end{aligned}$$

Here, e.g.,

$$\begin{aligned}
A_{JK4; J' K' 4} &= \langle 0_- (J K) | A | 0_- (J' K') \rangle \\
&= \frac{1}{2} (- \langle J K | + \langle J-K |) A (- |J' K' \rangle + |J'-K' \rangle) \\
&= \frac{1}{2} \{ A_{JK; J' K} + A_{J-K; J'-K} \} \delta_{K, K'} \\
&= A_{JK; J' K} \delta_{K, K'} \text{ for } \Delta J = J - J' = 0, \pm 2 \quad (17a)
\end{aligned}$$

$$= 0 \text{ for } \Delta J = \pm 1. \quad (17b)$$

The results for all other A and B matrix elements can be obtained in a similar fashion, and it may readily be verified that the non-vanishing matrix elements of both A and B obey the selection rules

$$E_+ \nleftrightarrow E_+, E_- \nleftrightarrow E_-, O_+ \nleftrightarrow O_+, O_- \nleftrightarrow O_- \text{ for } \Delta J = 0, \pm 2,$$

$$E_+ \nleftrightarrow E_-, O_+ \nleftrightarrow O_- \text{ for } \Delta J = \pm 1.$$

That there are no allowed matrix elements between even and odd states follows from Eqs. (9) since  $\Delta K = K - K'$  is always even.

We now define

$$\begin{aligned}
A_{J\tau v; J'\tau'v'} &= \\
&\sum_{KK'} \langle J \tau v | J K v \rangle A_{JKv; J' K' v'} \langle J' K' v' | J' \tau' v' \rangle, \quad (18a)
\end{aligned}$$



$$B_{J\tau\nu;J'\tau'\nu'} =$$

$$\sum_{KK'} \langle J \tau \nu | J K \nu \rangle B_{JK\nu;J'K'\nu'} \langle J' K' \nu' | J' \tau' \nu' \rangle. \quad (18b)$$

These matrices satisfy sum rules similar to Eqs. (10), in particular

$$\sum_{J'\tau'\nu'} A_{J\tau\nu;J'\tau'\nu'}^2 = \sum_{J'\tau'\nu'} B_{J\tau\nu;J'\tau'\nu'}^2 = 1, \quad (19a)$$

$$\sum_{J'\tau'\nu'} A_{J\tau\nu;J'\tau'\nu'} B_{J\tau\nu;J'\tau'\nu'} = 0. \quad (19b)$$

In terms of these matrices, Eq. (16) assumes its final form

$$\begin{aligned} \langle J \tau \nu | | Q^t | | J' \tau' \nu' \rangle &= (-1)^{J+J'} \\ &\cdot \left\{ \left( Q_{zz}^t - \frac{1}{2} Q_{xx}^t - \frac{1}{2} Q_{yy}^t \right) A_{J\tau\nu;J'\tau'\nu'} \right. \\ &\left. - \frac{3}{4} (Q_{xx}^t - Q_{yy}^t) B_{J\tau\nu;J'\tau'\nu'} \right\}. \end{aligned} \quad (20)$$

Programs to compute the A, B matrices for H<sub>2</sub>O and other asymmetric rotor molecules have been written and are presently operational. These programs operate as subroutines which are attached to programs, developed at AFGL, which generate the eigenvalues and eigenvectors of the asymmetric rotor Hamiltonian. These latter programs also include vibrational-rotational coupling via the Watson Hamiltonian method. The programs are quite efficient, requiring approximately 60 seconds of CP time to compute the strongest ( $\Delta K_a = 0, \pm 2$ ) quadrupole transitions for  $J \leq 22$ . A program listing of our quadrupole moment subroutines is furnished in Appendix C of the present report.

Numerical results for the A, B matrix elements in Eq. (20) are presented in Appendix B for some low J quadrupole transitions. The labeling of the  $K_a, K_c$  states in the tabulation of Appendix B is consistent with a IR symmetric top representation for H<sub>2</sub>O. We have verified that our methods do give representation-independent results, in the sense that

the same matrix element  $\langle J \tau || Q^t || J' \tau' \rangle$  always corresponds to the same energies  $E_{J\tau}$ ,  $E_{J'\tau'}$ , and energy difference  $E_{J\tau} - E_{J'\tau'}$ . However, if one switches representations, e.g. from IR to IIR, the  $K_a$ ,  $K_c$  labeling of the states also switches, as discussed in Allen and Cross.<sup>16/</sup>

Finally, to compute  $\langle J \tau || Q^t || J' \tau' \rangle$ , one needs to know values of  $Q_{xx}^t$ ,  $Q_{yy}^t$ ,  $Q_{zz}^t$  (which, again, are not all independent since  $\text{Tr}(Q^t) = 0$ ). For  $H_2O$  there appears to be no experimental determination of these quantities, however, Stogryn and Stogryn<sup>17/</sup> have listed fairly consistent theoretical values from quantum mechanical calculations. Their values are also quoted relative to the center of mass of the molecule. From Table 3 of Ref. 17 we deduce the following average values:

$$Q_{xx}^t = .12 \times 10^{-26} \text{ esu-cm}^2$$

$$Q_{yy}^t = -.72 \times 10^{-26} \text{ esu-cm}^2$$

$$Q_{zz}^t = .60 \times 10^{-26} \text{ esu-cm}^2$$

In order to make a simple comparison with the  $N_2$  quadrupole moment, we note from Eqs. (19), (20) that

$$\begin{aligned} \sum_{J', \tau'} |\langle J \tau || Q^t || J' \tau' \rangle|^2 \\ = (Q_{zz}^t - \frac{1}{2} Q_{xx}^t - \frac{1}{2} Q_{yy}^t)^2 + \frac{3}{4} (Q_{xx}^t - Q_{yy}^t)^2 \\ = 1.34 \times 10^{-52} \text{ (from values listed above).} \end{aligned}$$

The corresponding result for  $N_2$  is

$$\begin{aligned} \sum_{J'} |\langle J || Q^t || J' \rangle|^2 &= (1.52 \times 10^{-26} \text{ esu-cm}^2)^2 \\ &= 2.31 \times 10^{-52}, \end{aligned}$$

where the numerical value has been taken from Table 1 of Ref. 17.

Since the strength of dipole-quadrupole scattering in pressure broadening theory is directly proportional to the quadrupole moment squared, we infer from the numbers given above that the strength of this type of scattering for  $\text{H}_2\text{O}-\text{H}_2\text{O}$  should be roughly 60% of the corresponding strength for  $\text{H}_2\text{O}-\text{N}_2$ . In turn, one knows from pressure broadening calculations that the  $\text{H}_2\text{O}-\text{N}_2$  dipole-quadrupole strength is typically 20% of the  $\text{H}_2\text{O}-\text{H}_2\text{O}$  dipole-dipole strength. On this simple basis we expect the  $\text{H}_2\text{O}-\text{H}_2\text{O}$  dipole-quadrupole collisions to contribute something like a 10% correction to the broadened halfwidths.

The effect of these collisions will sometimes be enhanced when resonant energy denominators occur in the theory, however, this enhancement cannot be estimated without performing detailed calculations. Preliminary results from our pressure broadening programs indicate that the dipole-quadrupole collisions for  $\text{H}_2\text{O}-\text{H}_2\text{O}$  are negligible at low  $J$ , while at high  $J$  ( $J \geq 12$ ) they can contribute 10-15% of the total linewidth. This suggests that other mechanisms such as exchange scattering need to be considered.

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A P P E N D I X    A

MATRIX ELEMENTS OF  $[\phi_{z\alpha}^2 - \frac{1}{3}]$

## APPENDIX A

### Matrix Elements of $[\phi_{Z\alpha}^2 - \frac{1}{3}]$

We wish to evaluate Eq. (7) by introducing a complete set

$$\sum_{JKm} |J K m\rangle \langle J K m| = 1$$

of symmetric top states. Since  $J, m$  are also good quantum numbers for the asymmetric rotor, we obtain

$$\begin{aligned} & \langle J \tau m | \hat{Q}_{ZZ}^{\dagger} | J' \tau' m \rangle \\ &= \sum_{\alpha=x,y,z} Q_{\alpha\alpha} \sum_{KK'} \langle J \tau m | J K m \rangle \langle J K m | [\phi_{Z\alpha}^2 - \frac{1}{3}] | J' K' m \rangle \\ & \quad \langle J' K' m | J' \tau' m \rangle. \end{aligned} \quad (A1)$$

The symmetric top wave functions have the form<sup>6/</sup>

$$\psi_{JKm}(\theta, \psi, \phi) = e^{im\phi} e^{iK\psi} f_{JKm}(\theta), \quad (A2)$$

where  $(\theta, \psi, \phi)$  are the three Euler angles.

The direction cosines  $(\phi_{Zx}, \phi_{Zy}, \phi_{Zz})$  can be expressed as<sup>18/</sup>

$$\begin{aligned} \phi_{Zz} &= \cos\theta \\ \phi_{Zx} &= \sin\theta \sin\psi \\ \phi_{Zy} &= \sin\theta \cos\psi \end{aligned} \quad (A3)$$

which are independent of  $\phi$ . It follows that

$$[\phi_{Zz}^2 - \frac{1}{3}] = \frac{2}{3} \sqrt{\frac{4\pi}{5}} Y_{20}(\theta, \psi), \quad (A4)$$

$$[\phi_{Zx}^2 - \frac{1}{3}] = -\frac{1}{3}\sqrt{\frac{4\pi}{5}} Y_{20}(\theta, \psi) - \sqrt{\frac{2\pi}{15}} (Y_{22}(\theta, \psi) + Y_{2-2}(\theta, \psi)) , \quad (A5)$$

$$[\phi_{Zy}^2 - \frac{1}{3}] = -\frac{1}{3}\sqrt{\frac{4\pi}{5}} Y_{20}(\theta, \psi) + \sqrt{\frac{2\pi}{15}} (Y_{22}(\theta, \psi) + Y_{2-2}(\theta, \psi)) , \quad (A6)$$

where the Y's are spherical harmonics with the Condon and Shortley choice of phases.

The matrix element which are needed in Eq. (A1) are readily obtained using the formula<sup>6/</sup>

$$\begin{aligned} & \langle J K m | Y_{jk}(\theta, \psi) | J' K' m' \rangle \\ &= (-1)^k \sqrt{\frac{2j+1}{4\pi}} \sqrt{\frac{2J'+1}{2J+1}} (J' j K' k | J' j J(k+K')) \delta_{K, k+K'} \\ & \cdot (J' j m' 0 | J' j J m') \delta_{m, m'} . \end{aligned} \quad (A7)$$



## A P P E N D I X   B

MATRIX ELEMENTS OF A AND B (EQS. 18-20) FOR  $H_2O$  IN A  
IR REPRESENTATION FOR SOME LOW J QUADRUPOLE TRANSITIONS.

# APPENDIX B

Matrix Elements of A and B (Eqs. 18-20) for H<sub>2</sub>O in a  
IR Representation for Some Low J Quadrupole Transitions.

(A and B elements are dimensionless and satisfy the  
sum rules in Eq. (19); energies are in units cm<sup>-1</sup>.)

J, K <sub>a</sub> , K <sub>c</sub>	J', K' <sub>a</sub> , K' <sub>c</sub>	E <sub>J</sub>	E <sub>J</sub> - E <sub>J'</sub>	$\langle J A J' \rangle$	$\langle J B J' \rangle$
0, 0, 0	2, 0, 2	00.00	- 70.09	.99040	.13822
0, 0, 0	2, 2, 0	00.00	-136.16	-.13822	.99040
1, 0, 1	1, 0, 1	23.79	00.00	-.63246	.00000
1, 0, 1	2, 2, 1	23.79	-111.11	.00000	-.81650
1, 0, 1	3, 0, 3	23.79	-112.97	.74391	.16089
1, 0, 1	3, 2, 1	23.79	-188.36	-.21586	.55448
1, 1, 0	1, 1, 0	42.37	00.00	.31623	-.54772
1, 1, 0	2, 1, 2	42.37	- 37.13	.70711	.40825
1, 1, 0	3, 1, 2	42.37	-130.99	.62988	-.11805
1, 1, 0	3, 3, 0	42.37	-243.05	-.05704	.72069
1, 1, 1	1, 1, 1	37.14	00.00	.31623	.54772
1, 1, 1	2, 1, 1	37.14	- 58.04	.70711	-.40825
1, 1, 1	3, 1, 3	37.14	-105.14	.63088	.23203
1, 1, 1	3, 3, 1	37.14	-248.08	-.04465	.69245

A P P E N D I X   C

PROGRAM LISTING OF QUADRUPOLE MOMENT SUBROUTINES

```

RUN(S,,1011,,,,77777)
ATTACH(SAC,ASMR0TUPDATE, ID=CLOUGH,MR=1.
UPDATE(P=SAC,F)
REWIND,COMPILE.
RUN(S,,,COMPILE)
RETURN,SAC,COMPILE.
ATTACH(SAC,QUADM, ID=DAVIES,MR=1.)
RUN(S,,,SAC)
LOSET(PRESET=INDEF)
MAP,PART.
REQUEST,TAPE8,*PF.
LOAD(LGO)
EXECUTE.
EXIT.

```

```

*ID QUADMO
*I ASMR0T.1
NOLIST

*I ASMR0T.18
COMMON/QUADOF/IFQDEV,IFQDOD
*I ASMR0T.46
READ(INTAPE,921) IFQDEV,IFQDOD
921 FORMAT(2I5)
*I ASMR0T.114
IF(IFQDEV.EQ.0) CALL QUADEV
IF(IFQDOD.EQ.0) CALL QUADOD

```



```

PROGRAM CRLAS (INPUT,OUTPUT,TAPE7,TAPE1,TAPE5=INPUT,TAPE6=OUTPUT,
1  TAPE2,TAPE8)
COMMON /XYZ/ INTAPE,LEAVE,JUGGLE,JPUNCH,LSTOR,LOUT,LTAPES(4)
COMMON/WRTCNT/IWRTCN
LOUT=6
JUGGLE=0
JUGGLE=6
JUGGLE=1
LSTOR=0
LSTOR=7
LSTOR=6
LSTOR=2
CALL FTNIN(1,0,CUMMY)
10 CONTINUE
INTAPE=5
JPUNCH=1
LEAVE=1
LEAVE=6
CALL ASMROT
WRITE(6,900) IWRTCN
900 FORMAT(10X,*IWRITECOUNT=*,I10)
C
CALL LSTSC
STOP
END
SUBROUTINE PHITOP (G,V)
DIMENSION G(39),V(39)
COMMON /CONSTID/ OPID(40),SYMID(40)
DATA (SYMID(I),I=1,39)
$ 6H 200 ,6H 110 ,6H 020 ,6H 101 ,6H 100 ,6H 0 ,6H 001 ,
$ 6H 300 ,6H 210 ,6H 120 ,6H 030 ,6H 011 ,6H 0 ,6H 021 ,
$ 6H 102 ,6H 012 ,6H 003 ,
$ 6H 040 ,6H 130 ,6H 220 ,6H 310 ,6H 050 ,6H 230 ,
$ 6H 320 ,6H 060 ,6H 150 ,6H 240 ,6H 030 ,6H 0 ,6H 090 /
$ 6H 031 ,6H 121 ,6H 211 ,6H 301 ,6H 041 ,6H 0 ,6H 090 /
DO 30 J=1,39

```



```

2      BOLTZ(31,4,2),MAT1(31,31),MAT2(31,31),MAT3(31,31),MAT4(31,31),000410
3      TJHI(31,31,4)000420
COMMON /INT/ ITEMP,TEMP(3),OSUM,BOTLIM,UPLIM,RFREQ,KDIP,000430
C      IDIP(3),DIPOLE(3),TPhi(9,3),DIPSQ(3)000440
COMMON /VECL0/ TJL0(31,31,4)000450
COMMON /XRC/ RC,RELO,SUMINT1,SUMINT2,SUMINT3000460
COMMON /FNG1/ EJ,P2,P4,P6000470
COMMON /SELEC/ XCIP,XTYP000480
COMMON/QUADOF/IFQDEV,IFQDOD000490
COMMON/QUADA/ KDIM3(4),LSYM3(4),AQD(31,31),BQD(31,31),WJL00(31,4),000500
1      HLAM03(31,4),BOLTZ3(31,4),TJL00(31,31,4)000510
IF(INDSUB(3).NE.0) GO TO 20000520
INDSUB(3)=1000530
CALL FREQ0(0,0,0,0,0)000540
READ(INTAPE,900) JFREM,N,JFREM,X,(IDIP(I),I=1,3),BOTLIM,UPLIM,RELOR000550
900 FORMAT(2I5,5X,3I5,2F10.3,E10.3)000560
IF(JFREM.NE.JMIN) JFREM=JMIN+1000570
IF(JFREM.GT.JMAX) JFREM=JMAX000580
IF(LOUT.EQ.JUGGLE) RETURN000590
20 CONTINUE000600
IF(JJ.LT.JFREM-1) RETURN000610
IF(JJ.LT.0) RETURN000620
IF(JJ.EQ.JMIN) WRITE(LOUT,901) JJ,JMIN,JMAX,JFREM,JFREM,X000630
901 FORMAT(10X,*JJ=*,I3,2X,*JMIN=*,I3,2X,*JMAX=*,I3,2X,*JFREM=*,I3,000640
1      2X,*JFREM=*,I3,2X,*FOR DELTAJ EVEN*)000650
JJ=0 GIVES NO MATRIX ELEMENTS000660
IF(JJ.EQ.0) RETURN000670
IF(JJ.EQ.JFREM) IFQDEV=1000680
QINTNS=JINTNS(L,LP,ITYPE)000690
FREQD=FREQD(L,LP,ITYPE,INCKPA,INCKPB) . THE LA TWO000700
PARAMETERS IN FREQD REPRESENT VALUES FOR THE A, R PICES WHICH000710
ENTER INTO SUBROUTINE CSOM13 IN THE FORM IDEL=(KD (NCKP)/2 .000720
CAUTION...INCKPA,INCKPB MUST BE EVEN. PRESENT P DURE000730
LIMITS TRANSITIONS TO DELTA(KA)=0,2,-2000735
DO JP=J TRANSITIONS FOR A AND R000740

```

```

C      IN JP=J CASE , A AND B ARE HERMITIAN , IT IS ONLY NECESSARY TO
C      CALL FREQ00 FOR INCKPA AND INCKE VALUES GREATER OR EQUAL ZERO.
C      CALL QINTNS(1,1,0)
C      DO STRONG (SYMMETRIC TOP) TRANSITIONS .
C      CALL FREQ00(1,1,0,0,2)
C      NOW ADD SOME WEAKER TRANSITIONS .
C      CALL FREQ00(1,1,0,2,0)
C      E- DOESNT EXIST FOR JJ LESS THAN OR EQUAL TO ONE .
C      IF(JJ.EQ.1) GO TO 85
C      CALL QINTNS(2,2,0)
C      DO STRONG (SYMMETRIC TOP) TRANSITIONS .
C      CALL FREQ00(2,2,0,0,2)
C      NOW ADD SOME WEAKER TRANSITIONS .
C      CALL FREQ00(2,2,0,2,0)
C      85 CONTINUE
C      CALL QINTNS(3,3,0)
C      DO STRONG (SYMMETRIC TOP) TRANSITIONS .
C      CALL FREQ00(3,3,0,0,2)
C      CALL FREQ00(3,3,0,-99,0)
C      NOW ADD SOME WEAKER TRANSITIONS .
C      CALL FREQ00(3,3,0,2,-99)
C      CALL QINTNS(4,4,0)
C      DO STRONG (SYMMETRIC TOP) TRANSITIONS .
C      CALL FREQ00(4,4,0,0,2)
C      CALL FREQ00(4,4,0,-99,0)
C      NOW ADD SOME WEAKER TRANSITIONS .
C      CALL FREQ00(4,4,0,2,-99)
C      IF(JJ.LT.JFREOMN+1) GO TO 2000
C      DO JP=J-2 TRANSITIONS FOR A,B .
C      SKIP CALCULATION FOR J=1 .
C      IF(JJ.LE.1) GO TO 2000
C      CALL QINTNS(1,1,2)
C      DO STRONG (SYMMETRIC TOP) TRANSITIONS .
C      CALL FREQ00(1,1,2,0,2)
C      CALL FREQ00(1,1,2,-99,-2)

```

```

000750
000760
000770
000780
000790
000800
000810
000830
000840
000850
000860
000870
000880
000890
000910
000920
000930
000940
000950
000960
000970
000980
000990
001000
001010
001020
001030
001040
001050
001060
001070
001080
001090
001100
001110

```



```

C      NOW ADD SOME WEAKER TRANSITIONS .
      CALL FREQ00(1,1,2,2,0)
      CALL FREQ00(1,1,2,-2,-99)
      E- DOESNT EXIST FOR JP=JJ-2=0
      IF(JJ.EQ.2) GO TO 88
      CALL QINTNS(2,2,2)
      DO STRONG (SYMMETRIC TOP) TRANSITIONS .
      CALL FREQ00(2,2,2,0,2)
      CALL FREQ00(2,2,2,-99,-2)
      NOW ADD SOME WEAKER TRANSITIONS .
      CALL FREQ00(2,2,2,2,0)
      CALL FREQ00(2,2,2,-2,-99)
      88 CONTINUE
      CALL QINTNS(3,3,2)
      DO STRONG (SYMMETRIC TOP) TRANSITIONS .
      CALL FREQ00(3,3,2,0,2)
      CALL FREQ00(3,3,2,-99,-2)
      CALL FREQ00(3,3,2,-99,0)
      NOW ADD SOME WEAKER TRANSITIONS .
      CALL FREQ00(3,3,2,2,-99)
      CALL FREQ00(3,3,2,-2,-99)
      CALL QINTNS(4,4,2)
      DO STRONG (SYMMETRIC TOP) TRANSITIONS .
      CALL FREQ00(4,4,2,0,2)
      CALL FREQ00(4,4,2,-99,-2)
      CALL FREQ00(4,4,2,-99,0)
      NOW ADD SOME WEAKER TRANSITIONS .
      CALL FREQ00(4,4,2,2,-99)
      CALL FREQ00(4,4,2,-2,-99)
      2000 CONTINUE
      RETURN
      END
      SUBROUTINE QUADOC
      COMMON /XYZ/ INTAPE, LEAVE, JUGGLE, JPUNCH, LSTOR, LO
      COMMON IFEDIG, IFTRPS, IFTROS, IFTRRW, -FTRQW, IFTXP
      TAPES(4)
      SUM, IFLIST,

```

```

001120
001130
001140
001170
001180
001190
001200
001210
001220
001230
001240
001250
001280
001290
001300
001310
001320
001330
001340
001350
001360
001390
001400
001410
001420
001430
001440
001450
001460
001490
001500
001510
001520
001530
001540

```

```

1 IFSTAR,IFCHOY,IFCLOK,IFPUNC,INDSUB(20) 001550
COMMON W0,CXX,CYY,CZ,T1,T2,T3,T4,T5,T6,PHI(30) 001560
COMMON R0C,COEEK,EMC,01,02,03,04,05,06,HH(30) 001570
COMMON JJ,JMIN,JMAX,JSYM,KOIM(4,2),LSYM(4,2),DEGEN(2),WJMAX 001580
COMMON NDIM,KP(31,4),KO(31,4),WJHI(31,4),WJLO(31,4),HLAMD(31,4,2), 001590
2 BOLTZ(31,4,2),MAT1(31,31),MAT2(31,31),MAT3(31,31),MAT4(31,31), 001600
3 TJHI(31,31,4) 001610
COMMON /INT/ ITEMP,TEMP(3),QSUM,BOTLIM,UPLIM,RFREG,KOIP, 001620
C IDIP(3),DIPOLE(3),DPHI(9,3),DIPSQ(3) 001630
COMMON/VECL0/TJLO(31,31,4) 001635
COMMON /XRC/ RC,RELO,SUMINT1,SUMINT2,SUMINT3 001640
COMMON /FN00/ EJ,P2,P4,P6 001650
COMMON /SELEC/ XDIP,XTYP 001660
COMMON/QUADOF/IFQDEV,IFQ000 001670
COMMON/QUAD/ KOIP3(4),LSYM3(4),A00(31,31),B00(31,31),WJL00(31,4), 001680
1 HLAMD3(31,4),BOLTZ3(31,4),TJL00(31,31,4) 001690
IF (INDSUB(2).NE.0) GO TO 20 001700
INDSUB(2)=1 001710
CALL FREQD(0,0,0,0,0) 001720
READ(INTAPE,900) JFREM,N,JFREM,N,(IDIP(I),I=1,3),BOTLIM,UPLIM,RELO 001730
900 FORMAT(2I5,5X,3I5,2F10.3,E10.3) 001740
IF (JFREM.NE.JMIN) JFREM=N+1 001750
IF (JFREM.GT.JMAX) JFREM=N+1 001760
IF (LOUT.EQ.JUGGLE) RETURN 001770
20 CONTINUE 001780
ONLY STORE FOR J=0,DON'T COMPUTE TRANSITIONS. 001790
IF (JJ.LT.JFREM) GO TO 4000 001800
IF (JJ.EQ.JMIN+1) WRITE(LOUT,901) JJ,JMIN,JMAX,JFREM,N,JFREM,N 001810
901 FORMAT(10X,*JJ=*,I3,2X,*JMIN=*,I3,2X,*JMAX=*,I3,2X,*JFREM=*,I3, 001820
1 2X,*JFREM=*,I3,2X,*FOR DELTAJ ODD*) 001830
J=1 GIVES NO DELTAJ=ODD TRANSITIONS.IF J=1 ONLY STORE 001840
IF (JJ.EQ.JFREM)GO TO 2000 001850
IF (JJ.EQ.JFREM) IFQ000=1 001860
DO JP=J-1 TRANSITIONS FOR A,B 001870
C E- DOESNT EXIST FOR JP=JJ-1=1 001880

```

001890  
001900  
001910  
001920  
001930  
001940  
001950  
001960  
001980  
001990  
002000  
002010  
002020  
002030  
002040  
002050  
002070  
002080  
002090  
002100  
002110  
002120  
002130  
002140  
002150  
002160  
002170  
002180  
002190  
002200  
002210  
002220  
002240  
002250  
002260

```

IF(JJ.LE.2) GO TO 85
CALL QINTNS(1,2,1)
DO STRONG (SYMMETRIC TOP) TRANSITIONS .
CALL FREQDD(1,2,1,0,2)
CALL FREQDD(1,2,1,-99,-2)
NOW ADD SOME WEAKER TRANSITIONS .
CALL FREQDD(1,2,1,2,0)
CALL FREQDD(1,2,1,-2,-99)
85 CONTINUE
CALL QINTNS(2,1,1)
DO STRONG (SYMMETRIC TOP) TRANSITIONS .
CALL FREQDD(2,1,1,0,2)
CALL FREQDD(2,1,1,-99,-2)
NOW ADD SOME WEAKER TRANSITIONS .
CALL FREQDD(2,1,1,2,0)
CALL FREQDD(2,1,1,-2,-99)
CALL QINTNS(3,4,1)
DO STRONG (SYMMETRIC TOP) TRANSITIONS .
CALL FREQDD(3,4,1,0,2)
CALL FREQDD(3,4,1,-99,-2)
CALL FREQDD(3,4,1,-99,0)
NOW ADD SOME WEAKER TRANSITIONS .
CALL FREQDD(3,4,1,2,-99)
CALL FREQDD(3,4,1,-2,-99)
CALL QINTNS(4,3,1)
DO STRONG (SYMMETRIC TOP) TRANSITIONS .
CALL FREQDD(4,3,1,0,2)
CALL FREQDD(4,3,1,-99,-2)
CALL FREQDD(4,3,1,-99,0)
NOW ADD SOME WEAKER TRANSITIONS .
CALL FREQDD(4,3,1,2,-99)
CALL FREQDD(4,3,1,-2,-99)
2000 CONTINUE
STORE SMALLER J EIGENVECTOR ARRAYS
IF(JJ.EQ.JFREM-1) GO TO 4000

```

002270  
002280  
002290  
002300  
002310  
002320  
002330  
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002470  
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002500  
002510  
002520  
002530  
002550  
002560  
002570  
002580  
002590  
002600  
002610  
002620

```

DO 3100 L=1,4
IF (LSYM(L,2).NE.C) GO TO 3100
LIM=KOIM(L,2)
LSYM3(L)=LSYM(L,2)
KOIM3(L)=KOIM(L,2)
IF (LIM.LT.1) GO TO 3100
DO 3020 I=1,LIM
WJLO(I,L)=WJLO(I,L)
HLAMD3(I,L)=HLAMD(I,L,2)
ROLT23(I,L)=ROLT7(I,L,2)
DO 3010 J=1,LIM
3010 TJL00(I,J,L)=TJL0(I,J,L)
3020 CONTINUE
3100 CONTINUE
4000 CONTINUE
DO 2100 L=1,4
IF (LSYM(L,1).NE.C) GO TO 2100
LIM=KOIM(L,1)
IF (LIM.LT.1) GO TO 2100
DO 2020 I=1,LIM
WJLO(I,L)=WJHI(I,L)
HLAMD(I,L,2)=HLAMD(I,L,1)
ROLT2(I,L,2)=ROLT7(I,L,1)
DO 2010 J=1,LIM
2010 TJL0(I,J,L)=TJHI(I,J,L)
2020 CONTINUE
2100 CONTINUE
RETURN
END
SUBROUTINE FREQC(L,LP,ITYPE,INCKPA,INCKPR)
COMMON /XY7/ INTAPE,LEAVE,JUGGLE,JPUNCH,LSTOR,LOUT,LTAPES(4)
COMMON IFEDIG,IFTRRS,IFTR0S,IFTRRW,IFTR0W,IFEXPP,IFPSUM,IFLIST,
1 IFSTAR,IFCHOY,IFCLOK,IFPUNC,INOSUB(20)
COMMON W0,CXX,CYY,CZ2,I1,I2,I3,I4,I5,I6,PHICON(30)
COMMON BPC,COEEK,BMC,D1,D2,D3,D4,D5,D6,HH(30)

```



```

COMMON JJ, JMIN, JMAX, JSYM, KDIM(4,2), LSYM(4,2), DEGEN(2), WJMAX 002630
COMMON NDIM, KP(31,4), KO(31,4), WJ(31,4,2), HLAM(31,4,2), 002640
1 BOLTZ(31,4,2), 002650
2 H(31,31), PHI(31,31), CO(31,31), MAT4(31,29), TENSIT(31), TENS2(31), 002660
3 TJHI(31,31,4) 002670
COMMON /VFCLO/ TJLO(31,31,4) 002680
COMMON /FN00/ EJ, P2, P4, P6 002690
COMMON /SELEC/ XDIP, XTP 002700
COMMON /INT/ ITEMF, TEMP(3), OSUM, BOTLIM, UPLIM, RFREQ, KDIP, 002710
C IDIF(3), DIPOLE(3), DPHI(9,3), DIPSQ(3) 002720
COMMON /XPC/ RC, RELO, SUMINT1, SUMINT2, SUMINT3 002730
COMMON /SSS/ SO(200), KPLO(4), KCOEL(4), XX11(4) 002740
COMMON/QUAD/ KDIM3(4), LSYM3(4), AQD(31,31), BQD(31,31), WJLO(31,4), 002750
1 HLAM(31,4), BOLTZ(31,4), TJLO(31,31,4) 002760
COMMON/WPTCNT/IMPTCN 002770
IF(INDSUB(10).NE.0) GO TO 70 002780
IWRICN=0 002790
INDSUB(10)=1 002800
READ(INTAPE,900) IPN,INTIND 002810
900 FORMAT(2I5) 002820
70 IF(L.LE.0) RETURN 002830
LO=ITYPE+1 002840
JP=JJ-ITYPE 002850
INCA=(KPLO(L)-KPLO(LP)+INCKPA)/2 002860
INC3=(KPLO(L)-KPLO(LP)+INCKPA)/2 002870
INCA, INC3 PLAY THE ROLE OF IDEL IN SUBROUTINE CSQM13 002880
IF(LO.EQ.3) GO TO 71 002890
IF((LSYM(L,1).NE.0).OR.(LSYM(LP,LO).NE.0)) RETURN 002900
GO TO 72 002910
71 IF((LSYM(L,1).NE.0).OR.(LSYM3(LP).NE.0)) RETURN 002920
72 CONTINUE 002930
MINA=1 002940
MINB=1 002950
IF(INCA.LT.0) MINA=1-INCA 002960
IF(INCB.LT.0) MINB=1-INCB 002970

```



```

LIM1=KDIM(L,1)
IF(LO.EQ.3) GO TO 73
LIM2=KDIM(LP,LO)
GO TO 74
73 LIM2=KDIM3(LP)
74 CONTINUE
MAXA=LIM1
MAXB=LIM1
IF(MAXA+INCA.GT.LIM2) MAXA=LIM2-INCA
IF(MAXR+INCB.GT.LIM2) MAXB=LIM2-INCB
JPKO=JP+KDEL(LP)
LTAUA=KP(MINA,L)-KO(MINA,L)
LTAUB=KP(MINB,L)-KO(MINB,L)
LLSYMA=((-1)*LTAUA+3)/2
LLSY4B=((-1)*LTAUB+3)/2
RENOA=SQRT(2.*JP+1)/SQRT(2.*JJ+1)
RENOB=RENOA/50(2+1)
IATYPE=1000
IBTYPE=2000
IF(INCKPA.EQ.-99) GO TO 590
IF(MINA.GT.MAXA) GO TO 590
DO 600 K=MINA,MAXA
KINC=K+INCA
HHI=WJ(K,L,1)
IF(LO.EQ.3) GO TO 500
HLO=WJ(KINC,LP,LO)
GO TO 501
500 HLO=WJL00(KINC,LP)
501 CONTINUE
C XLINE IS NOW THE FREQUENCY .
C XLINE=HHI-HLO
C WE COMPARE XLINE WITH THE UPPER AND LOWER LIMITS AND DISCARD
C IF IT DOES NOT PASS THE TESTS .
C ABSLIN=ARS(XLINE)
C IF((ABSLIN.LT.BOTLIM).OR.(ABSLIN.GT.UPLIM)) GO TO 590

```

```

002980
002990
003000
003010
003020
003030
003040
003050
003060
003070
003080
003090
003100
003110
003120
003130
003140
003150
003160
003170
003180
003190
003200
003210
003220
003230
003240
003250
003260
003270
003280
003290
003300
003310
003320

```

```

003330 KPP=KP(K,L)+INCKPA
003340 KOP=JPKO-KPP
003350 IF(KPP.LT.0.OR.KOP.LT.0) GO TO 600
003355 IF(KPP.GT.JP.OR.KOP.GT.JP) GO TO 600
003360 IF(IFLIST.NE.0) RETURN
003370 C OBTAIN A RESULTS FOR JP=J
003380 IF(ITYPE.EQ.0) AWIG=TRANSM(K,KINC,TJHI,AQD,TJHI,L,LIM1,LP,LIM2)
003390 C OBTAIN A RESULTS FOR JP=J-1
003400 IF(ITYPE.EQ.1) AWIG=TRANSM(K,KINC,TJHI,AQD,TJLO,L,LIM1,LP,LIM2)
003410 C OBTAIN A RESULTS FOR JP=J-2
003420 IF(ITYPE.EQ.2) AWIG=TRANSM(K,KINC,TJHI,AQD,TJLO,L,LIM1,LP,LIM2)
003430 IF(AWIG.EQ.0.0) GO TO 600
003440 C OBTAIN REVERSED MATRIX ELEMENT
003450 C FIRST CHECK THAT REVERSED MATRIX ELEMENT IS NOT A REPEAT .
003460 IHI=KO(K,L)+1000*KP(K,L)+1000000*JJ
003470 ILO=KOP+1000*KPP+1000000*JP
003480 IF(ILO.EQ.IHI) GO TO 51
003490 AWIGRV=((1)*ITYPE)*AWIG
003500
003510
003520
003530
003540
003550
003560
003570
003580
003590
003600
003610
003620
003630
003640
003650
003660

51 CONTINUE
AWIG=RENOA*AWIG
C SQUARE MATRIX ELEMENTS TO GIVE A MATRIX LINE STRENGTHS .
AWIG2=AWIG**2
IF(ILO.EQ.IHI) GO TO 52
AWIG2=AWIGRV**2
52 CONTINUE
WRITE(8) IATYPE,JJ,KP(K,L),KO(K,L),JP,KPP,KOP,XLINE,HI,
1 AWIG,AWIG2
WRITE(LEAVE,904) IATYPE,JJ,KP(K,L),KO(K,L),JP,KPP,KOP,XLINE,HHI,
1 AWIG,AWIG2
IWRTCN=IWRTCN+1
904 FORMAT(10X,I5,3X,3I3,4X,3I3,4(2X,E15.5))
IF(ILO.EQ.IHI) GO TO 507
C WRITE REVERSED TRANSITION
XLINE=-XLINE
WRITE(8) IATYPE,JP,KPP,KOP,JJ,KP(K,L),KO(K,L),X HLO,

```

```

1  AWIGRV,AWIGR2
WRITE(LEAVE:9C4) IATYPE,JP,KPP,KOP,JJ,KP(K,L),XO(K,L),XLINE,HLC,
1  AWIGRV,AWIGF2
IWRTCN=IWRTCN+1
600 CONTINUE
590 CONTINUE
IF(INCKPB.EQ.-99) GO TO 850
IF(MINB.GT.MAXB) RETURN
DO 800 K=MINB,MAXB
KINC=K+INCB
HHI=WJ(K,L,1)
IF(LO.EQ.3) GO TO 700
HLO=WJ(KINC,LP,LO)
GO TO 701
700 HLO=WJLOO(KINC,LP)
701 CONTINUE
C  XLINE IS NOW THE FREQUENCY .
C  XLINE=HHI-HLO
C  WE COMPARE XLINE WITH THE UPPER AND LOWER LIMITS AND DISCARD
C  IT IF IT DOES NOT PASS THE TESTS .
ABS LIN=ABS(XLINE)
IF((ABS LIN.LT.BOT LIM).OR.(ABS LIN.GT.UPLIM)) RETURN
KPP=KP(K,L)+INCKPB
KOP=JPKO-KPP
IF(KPP.LT.0.OR.KOP.LT.0) GO TO 800
IF(KPP.GT.JP.OR.KOP.GT.JP) GO TO 800
IF(IFLIST.NE.0) RETURN
C  OBTAIN B RESULTS FOR JP=J
IF(IATYPE.EQ.0) BWIG=TRANSM(K,KINC,TJHI,800,TJHI,L,LIM1,LP,LIM2)
C  OBTAIN B RESULTS FOR JP=J-1
IF(IATYPE.EQ.1) BWIG=TRANSM(K,KINC,TJHI,800,TJLO,L,LIM1,LP,LIM2)
C  OBTAIN B RESULTS FOR JP=J-2
IF(IATYPE.EQ.2) BWIG=TRANSM(K,KINC,TJHI,800,TJLO,L,LIM1,LP,LIM2)
IF(BWIG.EQ.0) GO TO 800
C  OBTAIN REVERSED MATRIX ELEMENT

```

```

C      FIRST CHECK THAT REVERSED MATRIX ELEMENT IS NOT A REPEAT .
      IHI=KO(K,L)+1000*KP(K,L)+1000000*JJ
      ILO=KOP+1000*KPP+1000000*JP
      IF(ILO.EQ.IHI) GO TO 61
      BWIGRV=(((-1)**ITYPE)*BWIG/SQ(2+1)
61 CONTINUE
      BWIG=RENOB*BWIG
C      SQUARE MATRIX ELEMENTS TO GIVE B MATRIX LINE STRENGTHS .
      BWIG2=BWIG**2
      IF(ILO.EQ.IHI) GO TO 62
      BWIGR2=BWIGRV**2
62 CONTINUE
      WRITE(R) IBTYPE, JJ, KP(K,L), KO(K,L), JP, KPP, KOP, XLINE, HHI,
1      BWIG, BWIG2
      WRITE(LEAVE, 904) IBTYPE, JJ, KP(K,L), KO(K,L), JP, KPP, KOP, XLINE, HHI,
1      BWIG, BWIG2
      IWRTCN=IWRTCN+1
      IF(ILO.EQ.IHI) GO TO 800
      WRITE REVERSED TRANSITION
      XLINE=-XLINE
      WRITE(8) IBTYPE, JP, KPP, KOP, JJ, KP(K,L), KO(K,L), XLINE, HLO,
1      BWIGRV, BWIGR2
      WRITE(LEAVE, 904) IBTYPE, JP, KPP, KOP, JJ, KP(K,L), KO(K,L), XLINE, HLO,
1      BWIGRV, BWIGR2
      IWRTCN=IWRTCN+1
800 CONTINUE
850 CONTINUE
      RETURN
      END
      FUNCTION TRANSM(I, J, UA, CO, UB, LA, LIMA, LB, LIMB)
      DIMENSION UA(31,31,4), CO(31,31), UB(31,31,4)
      AA=0.
      DO 20 IA=1, LIMA
      BB=0.
      DO 10 IB=1, LIMB

```



```

10 B3=B9+CO(IA,IB)*UB(IB,J,LR)
20 AA=AA+UA(IA,I,LA)*82
   TRANSM=AA
   RETURN
   END
   SUBROUTINE QINTNS(LA,LB,ITYPE)
   COMMON /XYZ/ INTAPE,LEAVE,JUGGLE,JPUNCH,LSTOR,LOUT,LTAPES(4)
   COMMON IFEDIG,IFIRQS,IFTRFS,IFTRRW,IFEXPP,IFFSUM,IFLIST,
1   IFSTAR,IFCHOY,IFCLOK,IFPUNC,INDSUB(20)
   COMMON W0,CXX,CYY,CZZ,T1,T2,T3,T4,T5,T6,PHICCN(30)
   COMMON BPC,COEEK,BMC,D1,D2,D3,D4,D5,D6,HH(30)
   COMMON JJ,JMIN,JMAX,JSYM,KDIM(4,2),LSYM(4,2),DEGEN(2),WJMAX
   COMMON NDIM,KP(31,4),KO(31,4),WJHI(31,4),WJLO(31,4),HLAMD(31,4,2),
2   BOLTZ(31,4,2),H(31,31),PHI(31,31),CO(31,31),MAT4(31,31),
3   TJHI(31,31,4)
   COMMON /INT/ ITEM,TEMP(3),QSUM,BOTLIM,UPLIM,RFREQ,KDIP,
   IDIF(3),DIPOLE(3),DPHI(9,3),DIPSQ(3)
   COMMON /SSS/ SQ(200),KPL0(4),KCDL(4),XX11(4)
   COMMON/QUAD/ KDIM3(4),LSYM3(4),AQD(31,31),BQD(31,31),WJLOO(31,4),
1   HLAMD3(31,4),BOLTZ3(31,4),TJLOO(31,31,4)
   IF(IFLIST.EQ.1) RETURN
   LO=ITYPE+1
   IF(LO.EQ.3) GO TO 50
   IF((LSYM(LA,1).NE.0).OR.(LSYM(LB,LO).NE.0)) RETURN
   LIMB=KDIM(LB,LO)
   GO TO 51
50 IF((LSYM(LA,1).NE.0).OR.(LSYM3(LB).NE.0)) RETURN
   LIMB=KDIM3(LB)
51 LIMA=KDIM(LA,1)
   CALL CSQM13(A00,E00,JJ,ITYPE,LA,LIMA,LB,LIMB)
   RETURN
   END
   SUBROUTINE CSQM13(A,P,J,ITYPE,L,LIM,L1,LIM1)
   SUBROUTINE CSQM13(A,B,J,ITYPE,L,LIM,L1,LIM1)
   PROGRAM SFTS UP THE WANG TRANSFORMED MATRICES

```





```

C      KP(I,L)=KPLO(L)+2.*(I-1)
C      CAUTION...IN THE PROGRAM KP(I,L) PLAYS THE ROLE OF K IN THE
C      COMMENT SECTION.
C      KPLO(1)=0 (E+), KPLO(2)=2 (E-), KPLO(3)=1 (O+) KPLO(4)=1 (O-)
C      THE ARRAYS ARE INITIALLY SET TO ZERO ,THUS ELEMENTS NOT
C      RESET REMAIN ZERO.
      DO 8 I1=1,31
      DO 8 I=1,31
      A(I,I1)=0.0
      B(I,I1)=0.0
      IF(J.EQ.0) GO TO 700
      KDEL=KPLO(L)-KPLC(L1)
      IF(ITYPE.EQ.1) GO TO 300
      DO DELTA(J) EVEN TRANSITIONS , THE SELECTION RULES FOR A,B ARE
      (O-,O-), (O+,O+), (E-,E-), (E+,E+)
      KDEL=0 THROUGHOUT THIS SECTION.
      JP=J-2
      IDEL=KDEL/2
      LIMLO=MAX0(1,1-IDEL)
      LIMHI=MIN0(LIM,LIM1-IDEL)
      IF(LIMHI.LT.LIMLO) GO TO 102
      DO 100 I=LIMLO,LIMHI
      I1=I+IDEL
      IF(ITYPE.EQ.2) GO TO 101
      DO JP=J TRANSITIONS FOR A MATRIX
      SNUM=3.*KP(I,L)**2-J*(J+1)
      NA=2*J-1
      NR=J
      NC=J+1
      ND=2*J+3
      REMEMBER SQ(I+1)=SQRT(I)
      DENOM=SQ(NA+1)*SQ(NB+1)*SQ(NC+1)*SQ(ND+1)
      GO TO 100
      DO JP=J-2 TRANSITIONS FOR A MATRIX
      101 IF(JP.LT.0) GO TO 102

```

005410  
005420  
005430  
005440  
005450  
005460  
005470  
005480  
005490  
005500  
005510  
005520  
005530  
005540  
005550  
005560  
005570  
005580  
005590  
005600  
005610  
005620  
005630  
005640  
005650  
005660  
005670  
005680  
005690  
005700  
005710  
005720  
005730  
005740  
005750

```

IA=JP-KP(I,L)+2
IB=JP-KP(I,L)+1
IC=JP+KP(I,L)+2
ID=JP+KP(I,L)+1
SNUM=SQ(3+1)*SQ(IA+1)*SQ(IC+1)*SQ(ID+1)
NA=2*JP+1
NB=2*JP+2
NC=2*JP+3
ND=JP+2
DENOM=SQ(NA+1)*SQ(NB+1)*SQ(NC+1)*SQ(ND+1)
100 A(I,I)=SNUM/DENOM
102 CONTINUE
C   OBTAIN 9(1,1) MATRIX ELEMENTS
    IF(L.EQ.1.OR.L.EQ.2)GO TO 106
    IF(ITYPE.EQ.2)GO TO 103
C   B(1,1) FOR JP=J
    SNUM=SQ(3+1)*SQ(J+1)*SQ(J+2)*SQ(J+1)*SQ(J+2)
    NA=2*J-1
    NB=J
    NC=2*J+2
    ND=2*J+3
    DENOM=SQ(NA+1)*SQ(NB+1)*SQ(NC+1)*SQ(ND+1)
    GO TO 105
C   B(1,1) FOR JP=J-2
103 IF(JP.LT.0) GO TO 106
    SNUM=SQ(JP+1)*SQ(JP+2)*SQ(JP+3)*SQ(JP+4)
    NA=2*JP+1
    NB=2*JP+2
    NC=2*JP+3
    ND=2*JP+4
    DENOM=SQ(NA+1)*SQ(NB+1)*SQ(NC+1)*SQ(ND+1)
105 B(1,1)=SNUM/DENOM
    IF(L.EQ.4) B(1,1)=-B(1,1)
106 CONTINUE
C   OBTAIN REMAINING B(I,I) MATRIX ELEMENTS

```

```

C FIRST DO UPPER SUPERDIAGONAL (K/K+2)
IDEL=(KOEL+2)/2
LIMLO=MAX0(1,1-IDEL)
LIMHI=MIN0(LIM,LIM1-IDEL)
IF(LIMHI.LT.LIMLO)GO TO 111
DO 110 I=LIMLO,LIMHI
I1=I+IDEL
IF(ITYPE.EQ.2) GO TO 108
C DO JP=J TRANSITIONS FOR B MATRIX
IA=J-KP(I,L)-1
IB=J-KP(I,L)
IC=J+KP(I,L)+1
ID=J+KP(I,L)+2
SNUM=SQ(3+1)*SQ(IA+1)*SQ(IB+1)*SQ(IC+1)*SQ(ID+1)
NA=2*J-1
NB=J
NC=2*J+2
ND=2*J+3
DENOM=SQ(NA+1)*SQ(NB+1)*SQ(NC+1)*SQ(ND+1)
GO TO 109
C DO JP=J-2 TRANSITIONS FOR B MATRIX
108 IF(JP.LT.0)GO TO 111
IA=JP-KP(I,L)-1
IB=JP-KP(I,L)
IC=JP-KP(I,L)+1
ID=JP-KP(I,L)+2
SNUM=SQ(IA+1)*SQ(IB+1)*SQ(IC+1)*SQ(ID+1)
NA=2*JP+1
NB=2*JP+2
NC=2*JP+3
ND=2*JP+4
DENOM=SQ(NA+1)*SQ(NB+1)*SQ(NC+1)*SQ(ND+1)
B(I,I1)=SNUM/DENOM
109
C INSERT WANG SORT(2) FACTOR FOR E+
110 IF(L.EQ.1.AND.I.EQ.1)B(I,I1)=SQ(2+1)*B(I,I1)

```



```

111      CONTINUE
C      NOW DO LOWER SUPERDIAGONAL
      IDEL=(KDEL-2)/2
      LIMLO=MAX0(1,1-IDEL)
      LIMHI=MIN0(LIM,LIM1-IDEL)
      IF(LIMHI.LT.LIMLO) GO TO 116
      DO 115 I=LIMLO,LIMHI
      I1=I-IDEL
      IF(ITYPE.EQ.2) GO TO 112
      DO JP=J TRANSITIONS FOR B MATRIX
      IA=J+KP(I,L)-1
      IB=J+KP(I,L)
      IC=J-KP(I,L)+1
      ID=J-KP(I,L)+2
      SNUM=SQ(3+1)*SQ(IA+1)*SQ(IB+1)*SQ(IC+1)*SQ(ID+1)
      NA=2*J-1
      NB=2*J
      NC=J+1
      ND=2*J+3
      DENOM=SQ(NA+1)*SQ(NB+1)*SQ(NC+1)*SQ(ND+1)
      GO TO 113
C      DO JP=J-2 TRANSITIONS FOR B MATRIX
      GO TO 112 IF(JP.LT.0) GO TO 116
      IA=JP+KP(I,L)-1
      IB=JP+KP(I,L)
      IC=JP+KP(I,L)+1
      ID=JP+KP(I,L)+2
      SNUM=SQ(IA+1)*SQ(IB+1)*SQ(IC+1)*SQ(ID+1)
      NA=2*JP+1
      NB=2*JP+2
      NC=2*JP+3
      ND=2*JP+4
      DENOM=SQ(NA+1)*SQ(NB+1)*SQ(NC+1)*SQ(ND+1)
      B(I,I1)=SNUM/DENOM
113      B(I,I1)=SNUM/DENOM
C      INSERT WANG SORT(2) FOR B+

```

```

006110
006120
006130
006140
006150
006160
006170
006180
006190
006200
006210
006220
006230
006240
006250
006260
006270
006280
006290
006300
006310
006320
006330
006340
006350
006360
006370
006380
006390
006400
006410
006420
006430
006440
006450

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```

115 IF(L.EQ.1.AND.I1.EQ.1) B(I,I1)=SQ(2+1)*R(I,I1)
116 CONTINUE
      GO TO 700
C     NOW DO DELTA(J) ODD TRANSITIONS, IN PARTICULAR DO JP=J-1
C     THE SELECTION RULES ARE (0+,0-), (0-,0+), (E+,E-), (E-,E+)
300 JP=J-1
C     J=1, JP=0 IS EXCLUDED
      IF(JP.LE.0) GO TO 700
      IOEL=KOEL/2
      LIMLO=MAX0(1,1-IDEL)
      LIMHI=MIN0(LIM,LIM1-IDEL)
      IF(LIMHI.LT.LIMLO) GO TO 401
      DO 400 I=LIMLO,LIMHI
        I1=I+IDEL
        OBTAIN JP=J-1 MATRIX ELEMENTS OF A
        IA=JP-KP(I,L)+1
        IB=JP+KP(I,6)+1
        SNUM=KP(I,L)*SQ(3+1)*SQ(IA+1)*SQ(IB+1)
        NA=JP
        NB=2*JP+1
        NC=JP+1
        ND=JP+2
        DENOM=SQ(NA+1)*SQ(NB+1)*SQ(NC+1)*SQ(ND+1)
        A(I,I1)=SNUM/DENOM
        CHANGE SIGN
        A(I,I1)=-A(I,I1)
400 CONTINUE
C     OBTAIN JP=J-1 MATRIX ELEMENTS OF B
C     FIRST OBTAIN B(1,1) MATRIX ELEMENT
      IF(L.EQ.1.OR.L.EQ.2) GO TO 406
      IA=JP
      IB=JP+1
      IC=JP+2
      ID=JP+1
      SNUM=SQ(IA+1)*SQ(IB+1)*SQ(IC+1)*SQ(ID+1)

```

```

006460
006470
006480
006490
006500
006510
006520
006530
006540
006550
006560
006570
006580
006590
006600
006610
006620
006630
006640
006650
006660
006670
006680
006690
006700
006710
006720
006730
006740
006750
006760
006770
006780
006790
006800

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006810  
006820  
006830  
006840  
006850  
006860  
006870  
006880  
006890  
006900  
006910  
006920  
006930  
006940  
006950  
006960  
006970  
006980  
006990  
007000  
007010  
007020  
007030  
007040  
007050  
007060  
007070  
007080  
007090  
007100  
007110  
007120  
007130  
007140  
007150

```

NA=JP
NB=2*JP+1
NC=JP+1
ND=2*JP+4
DENOM=SQ(NA+1)*SQ(NB+1)*SQ(NC+1)*SQ(ND+1)
B(1,1)=SNUM/DENOM
IF(L.EQ.3) B(1,1)=-B(1,1)
4J6 CONTINUE
C OBTAIN REMAINING B MATRIX ELEMENTS
C FIRST DO UPPER SUPERDIAGONAL
IDEL=(KDEL+2)/2
LIMLO=MAX0(1,1-IDEL)
LIMHI=MIN0(LIM,LIM1-IDEL)
IF(LIMHI.LT.LIMLO) GO TO 411
DO 410 I=LIMLO,LIMHI
I1=I-IDEL
IA=JP-KP(I,I)-1
I3=JP-KP(I,I)
IC=JP-KP(I,I)+1
ID=JP+KP(I,I)+2
SNUM=SQ(IA+1)*SQ(IB+1)*SQ(IC+1)*SQ(ID+1)
NA=JP
NB=2*JP+1
NC=JP+1
ND=2*JP+4
DENOM=SQ(NA+1)*SQ(NB+1)*SQ(NC+1)*SQ(ND+1)
B(I,I1)=SNUM/DENOM
C INSERT WANG SORT(2) FACTOR
C IF(L.EQ.1.AND.I.EQ.1) B(I,I1)=SQ(2+1)*B(I,I1)
C CHANGE SIGNS
410 B(I,I1)=-B(I,I1)
411 CONTINUE
C NOW DO LOWER SUPERDIAGONAL
IDEL=(KDEL-2)/2
LIMLO=MAX0(1,1-IDEL)

```

007160  
007170  
007180  
007190  
007200  
007210  
007220  
007230  
007240  
007250  
007260  
007270  
007280  
007290  
007300  
007310  
007320  
007330  
007340  
007350  
007360  
007370

```

LIMHI=MINO(LIM,LIM1-IDEL)
IF(LIMHI.LT.LIMLO) GO TO 700
DO 415 I=LIMLO,LIMHI
  I1=I+IDEL
  IA=JP+KP(I,L)-1
  IB=JP+KP(I,L)
  IC=JP+KP(I,L)+1
  ID=JP-KP(I,L)+2
  SNUM=-SQ(IA+1)*SQ(IB+1)*SQ(IC+1)*SQ(ID+1)
  NA=2*JF
  NB=JP+1
  NC=JP+2
  ND=2*JP+1
  DENOM=SQ(NA+1)*SQ(NB+1)*SQ(NC+1)*SQ(ND+1)
  B(I,I1)=SNUM/DENOM
  INSERT WANG SGR(2) FACTOR
  IF(L.EQ.2.AND.I.EQ.1) B(I,I1)=SQ(2+1)*B(I,I1)
  CHANGE SIGN
  C 415 B(I,I1)=-B(I,I1)
  700 CONTINUE
  RETURN
  END

```